



Institut für Thermische Strömungsmaschinen

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DNS and Embedded DNS as Tools for Investigating Unsteady Heat Transfer Phenomena in Turbines

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Collaborators:

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Universität Karlsruhe (TH)

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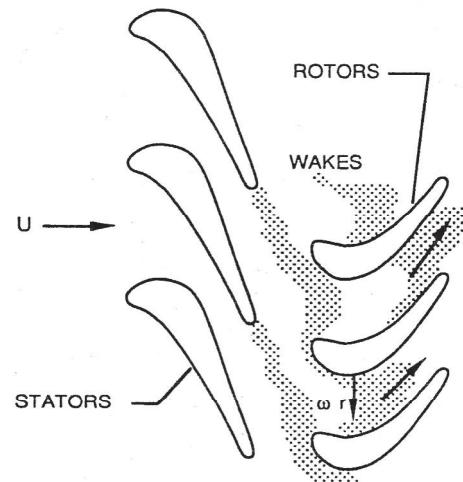




Classical DNS for Turbomachinery

Laminar-turbulent transition of a boundary layer on a compressor blade:

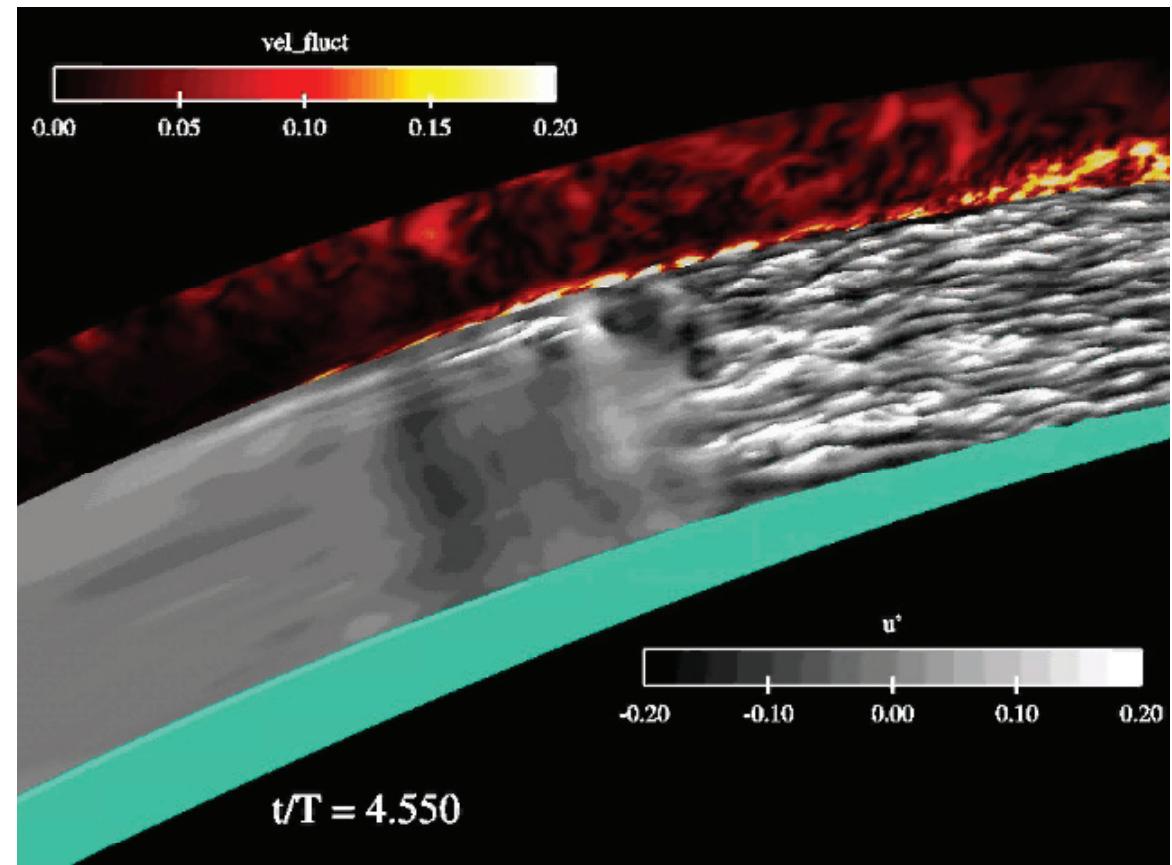
Development of turbulence in the boundary layer is accelerated by wakes of the approach flow



u-fluctuations

Red: Wakes

Gray: Boundary layer
(turbulent spots)



Rodi et al. (2007)

Dominic von Terzi - Minnowbrook VI, 24 August 2009

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Drawbacks of classical DNS

Demands on computer resources are extremely high!

Computational costs of some examples:

- Turbine blade (Wissink & Rodi, 2006):

93.4 million cells

240 000 time steps

512 000 CPU-hours on

Hitachi SR8000-F1

ca. 3 months on 256 CPUs

- Compressor blade (Rodi et al., 2007):

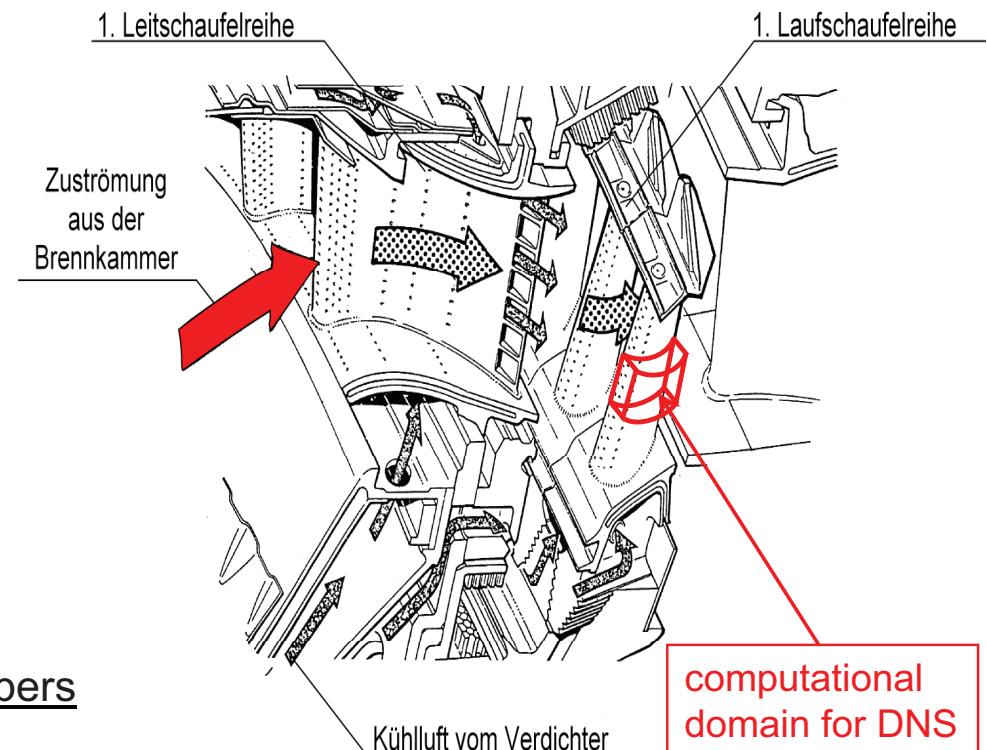
85 million cells

256 000 time steps

31 000 CPU-hours on NEC SX-8

ca. 20 days on 64 CPUs

⇒ So far only idealized configurations,
small domains and low Reynolds numbers



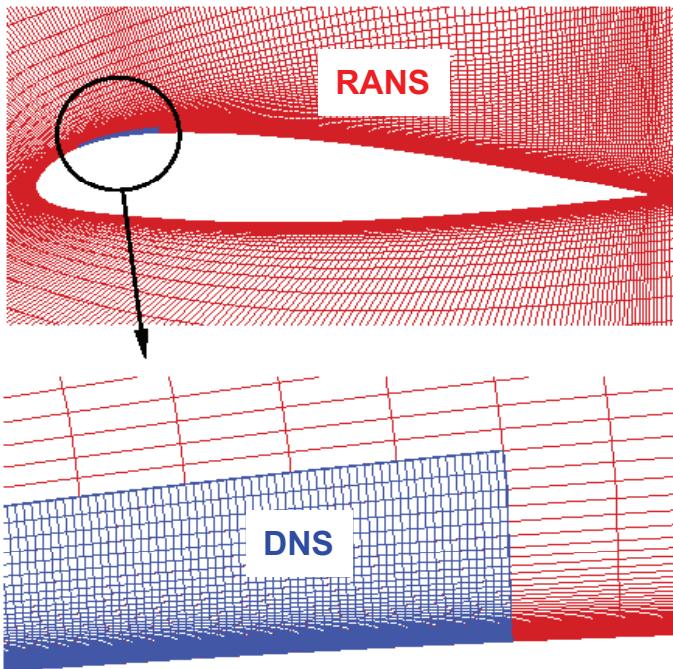
Proposed remedy:

Development of an “**embedded DNS**“ method
(DNS domain enclosed in RANS / LES domains)



The case for “embedded DNS”

Illustration: DNS-zone embedded in RANS-domain for better prediction of laminar-turbulent transition of the flow over an airfoil



Advantage:

RANS on coarser 2D grid, fine 3D grid for **DNS only in small sub-domain**
⇒ Immense reduction in computational cost

Required development of new technique:

Different **demands on numerical methods** in RANS and DNS areas
⇒ Adjustment of the flow solver

Key problem: Coupling at **interfaces**

⇒ Physically meaningful fluctuations required for DNS-boundaries (RANS delivers only mean values and LES only large-scale fluctuations!)

→ Can learn from **suitable** hybrid LES/RANS methods

von Terzi & Fröhlich (TSFP-5 2007, ETMM-7 2008), review: Fröhlich & von Terzi (JPAS, 2008)

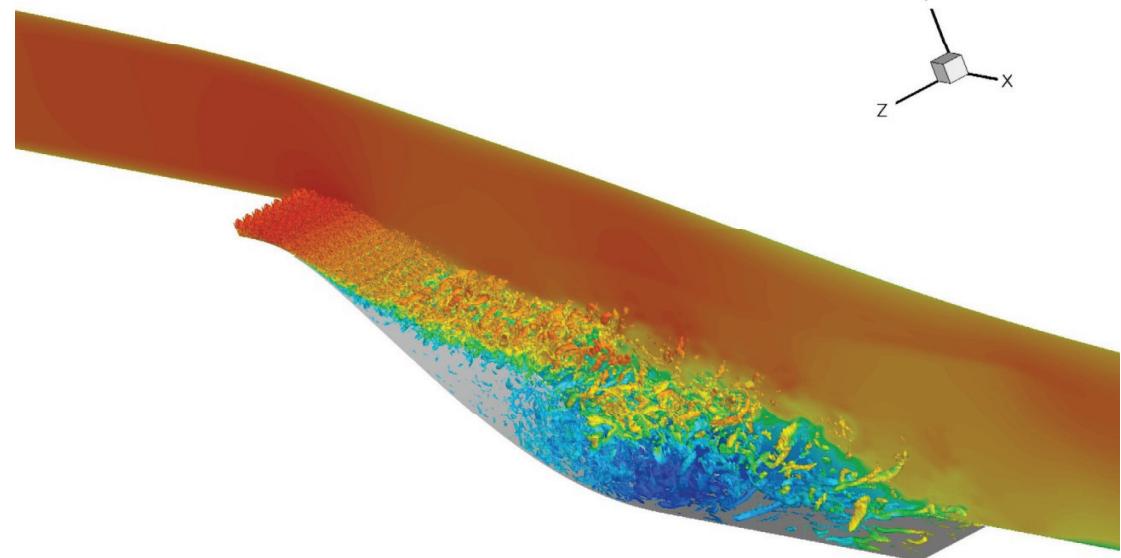
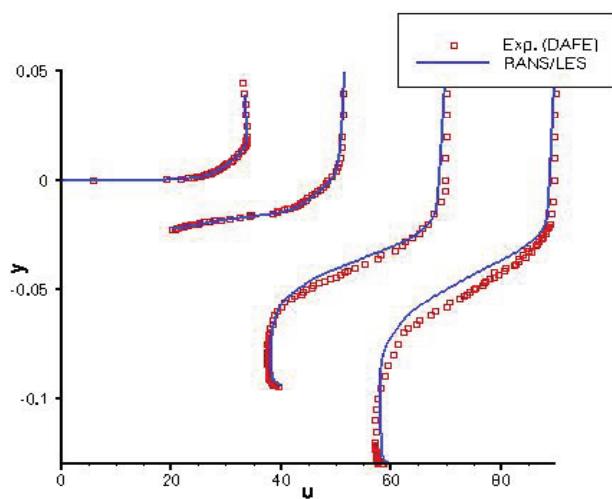


Illustrating example: Embedded LES

Separated flow in an asymmetric air intake:

Dilemma: Approach boundary layer at high Reynolds number **too costly for LES**, whereas separated flow region **poorly predicted by standard RANS methods**

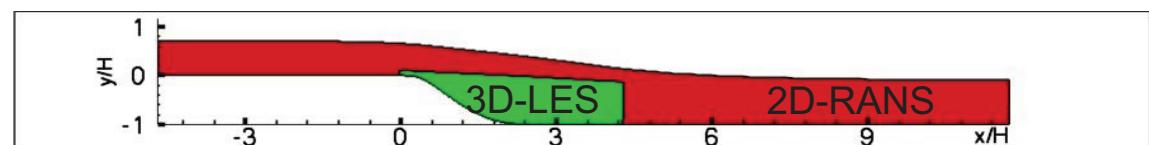
Re=400,000; 9.2 million cells



Vortex identification by Q-criterion

Generation of fluctuations:

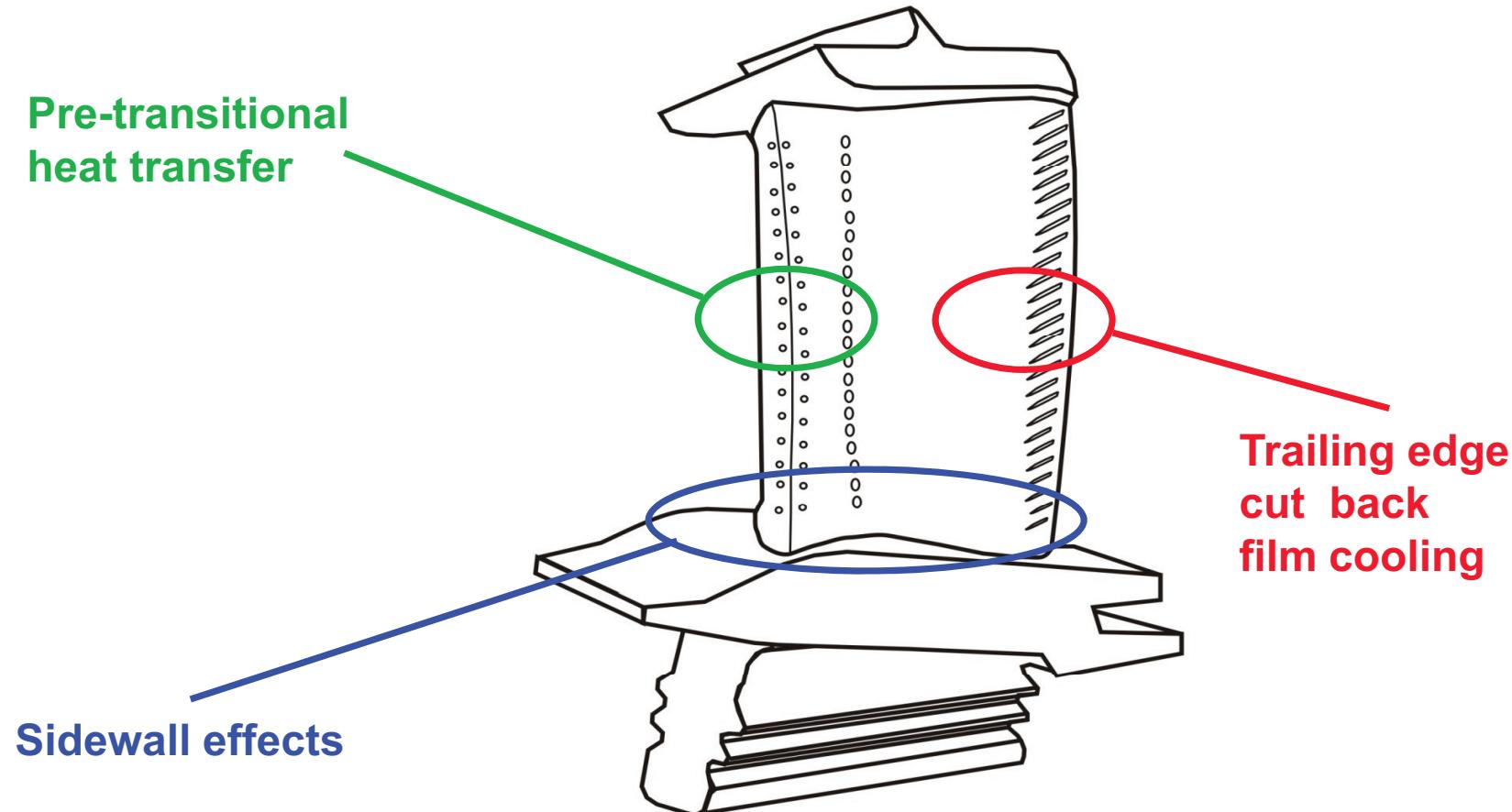
- inflow: database
- other boundaries: enrichment



courtesy of I. Mary, ONERA (see also v. Terzi, Fröhlich & Mary, inSiDE 2009)



Candidates for (embedded) DNS studies in turbines



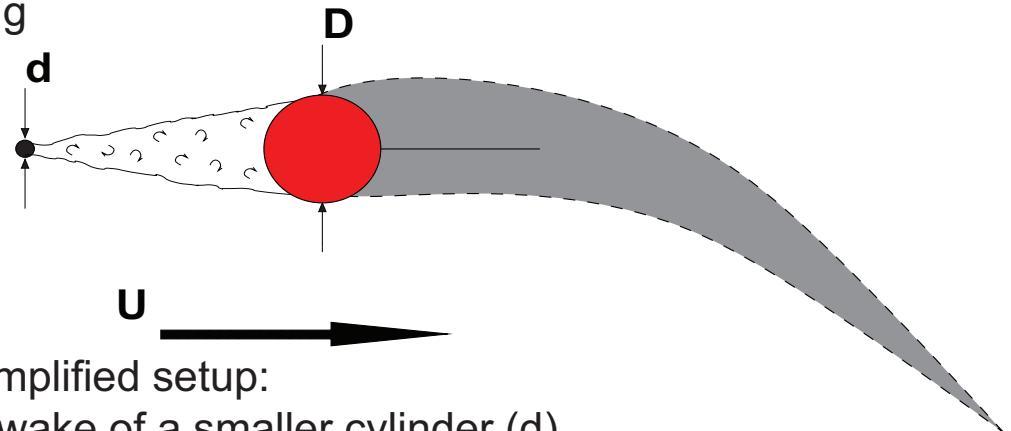
Mid-term goal: integrate in a complete turbine blade simulation with embedded DNS

Project: Pre-transitional heat transfer

with Venema & Rodi

Motivation:

- Increase in heat transfer at stagnation point of turbine blades due to incoming wakes and turbulence
- Physical mechanism unclear
- Predictions with RANS inaccurate and not reliable



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First step:

Reproduce experimental results for a simplified setup:

A larger cylinder (D) is immersed in the wake of a smaller cylinder (d)

$Re_D = 48,000$ (Magari & LaGraff, *J. Turbomachinery* 1994)

Second step:

Reproduce selected experimental results for a turbine blade

Third step:

Own numerical experiments to understand mechanism

→ better prediction of heat transfer



Project: Pre-transitional heat transfer

with Venema & Rodi

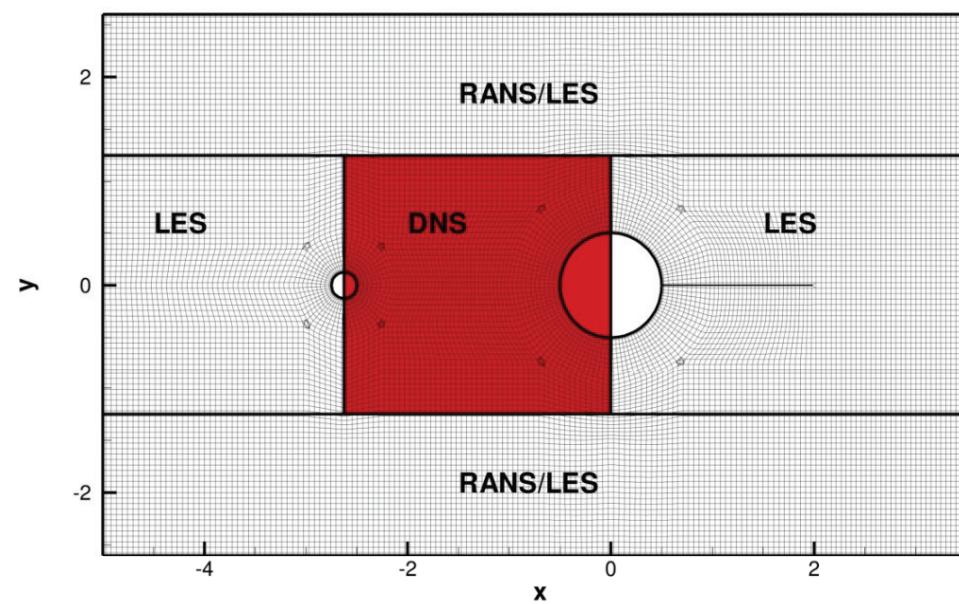
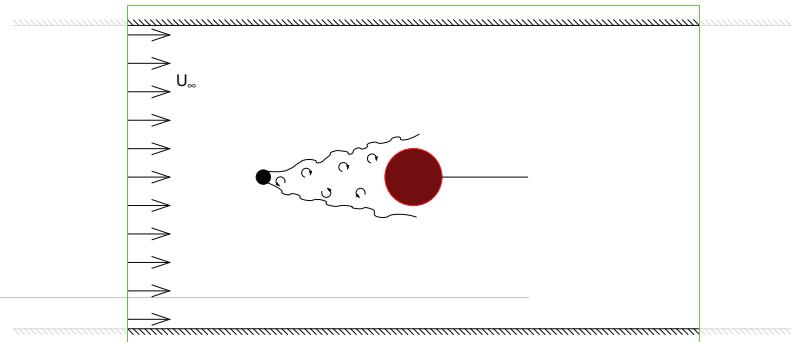
Schematic of setup for embedded DNS

Preliminary simulations:

$Re_D = 48,000$; 2 domain widths (2.5D & 1D);
each ca. 40 million cells, almost all in DNS region (in red)

Final simulations:

Estimated 200 & 800 million cells

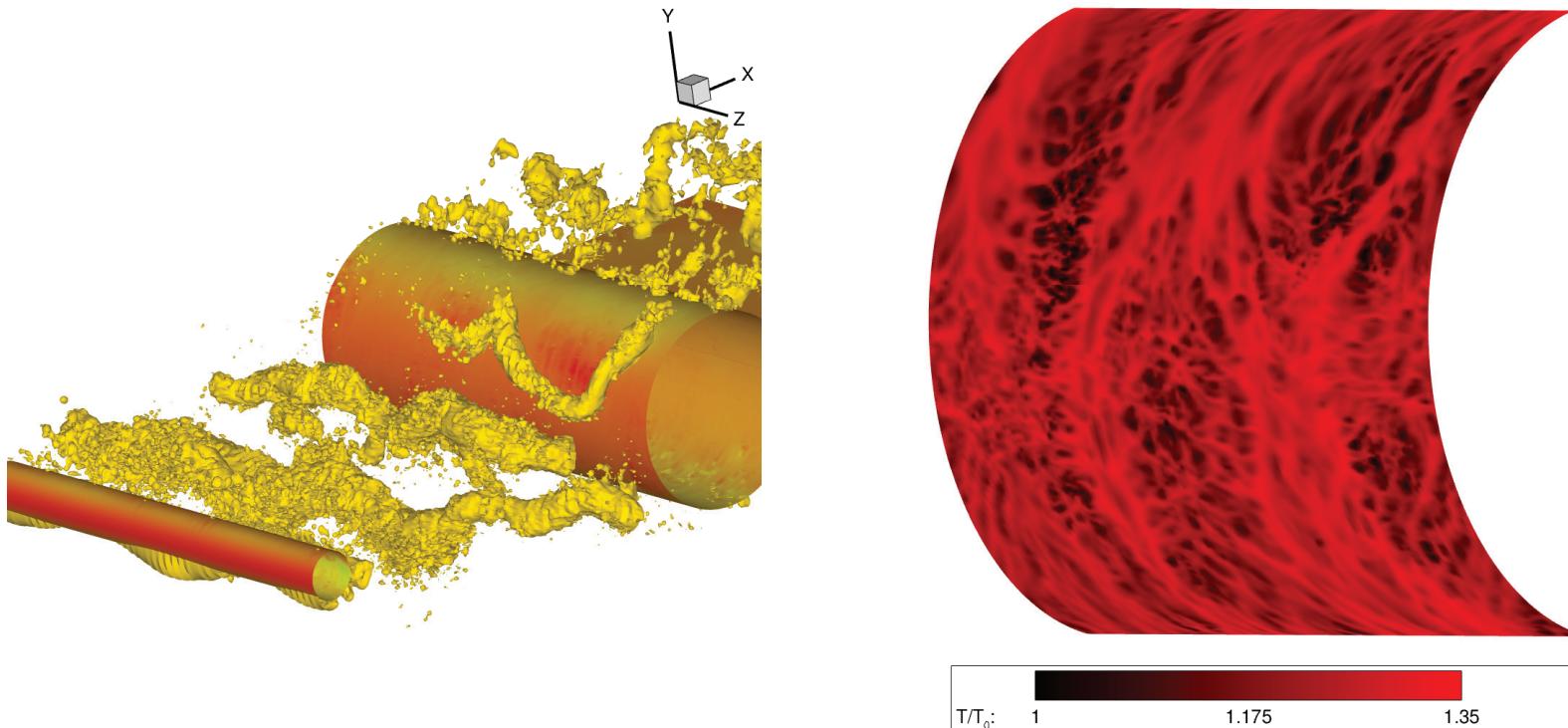




Project: Pre-transitional heat transfer

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Preliminary DNS results: wake induced temperature fluctuations



Iso-contours of instantaneous **pressure fluctuations** and **temperature** at cells adjacent to cylinders (full domain width of experiments 2.5 D)

Instantaneous **temperature** contours at stagnation point of large (heated) cylinder (higher resolution, but narrower domain width)

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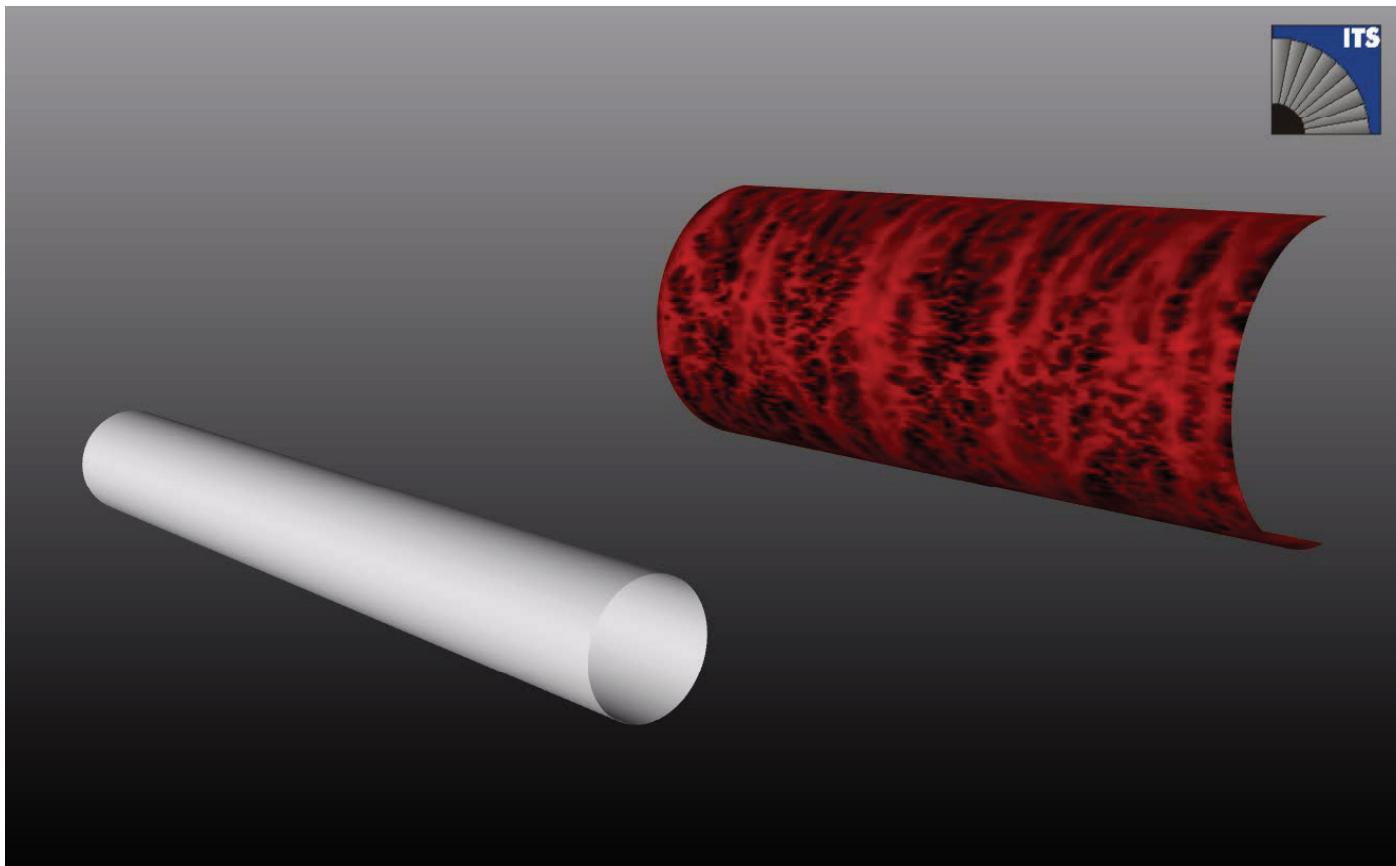
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Instantaneous temperature contours (wall-adjacent cell at large heated cylinder)



Coarse simulation of full domain width

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filename: 03dc_temp_rot.avi



Project: Trailing-edge cutback film-cooling

with Schneider & Bauer

Motivation:

Cooling film degradation due to enhanced mixing, presumably caused by large coherent structures, but exact mechanism unclear (competing mechanisms that can be exploited by flow control ?)

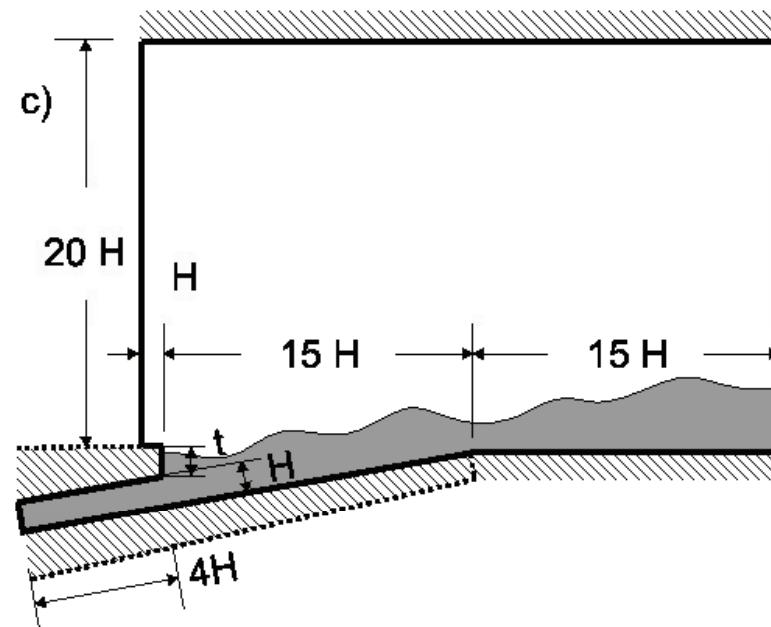
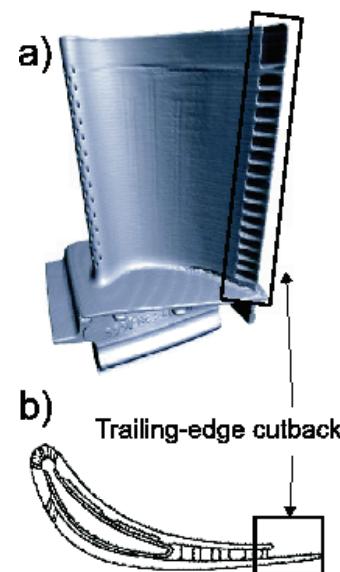
Focus here: IMPACT OF LOW BLOWING RATIO AND STATE OF COOLANT FLOW

$Re_H = 6,250$

$T_c/T_h = 0.75$

2 blowing ratios selected:
 $M=0.5$ & 1.1 (but velocity ratio matched !)

fully developed turbulent &
laminar coolant flows
simulated



Experiments of AITEB-1/2 by Martini, Schulz & Bauer (J. Turbomachinery 2006) and Martini (2008)

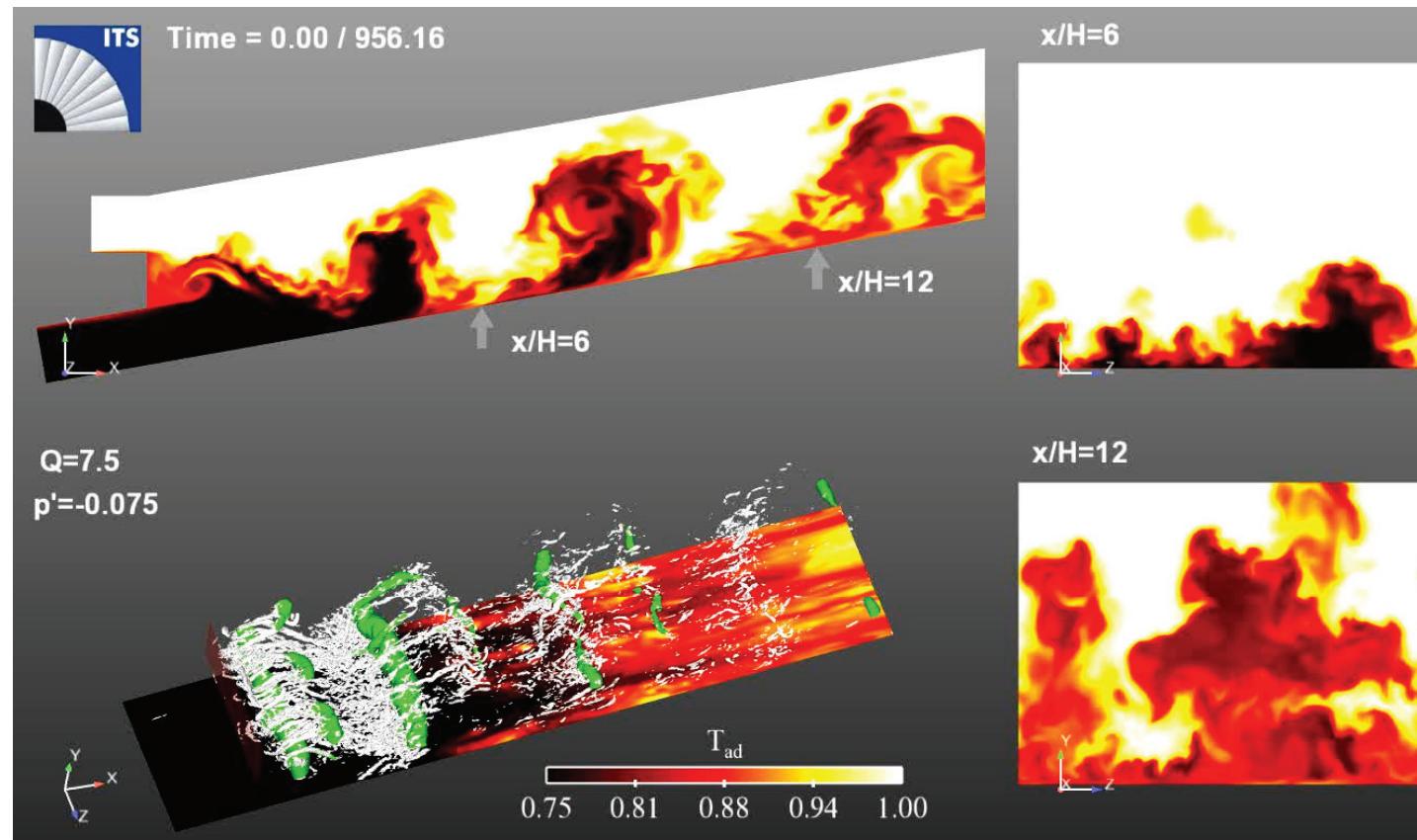
Preliminary “LES” study (ca. 14 million cells, incompressible) with vanishing model contribution
Schneider, v. Terzi & Bauer (THMT-6 2009)



Project: Trailing-edge cutback film-cooling

with Schneider & Bauer

Impact of coherent structures on the instantaneous flow and temperature field at the cutback for **high blowing ratio** with turbulent coolant ejection



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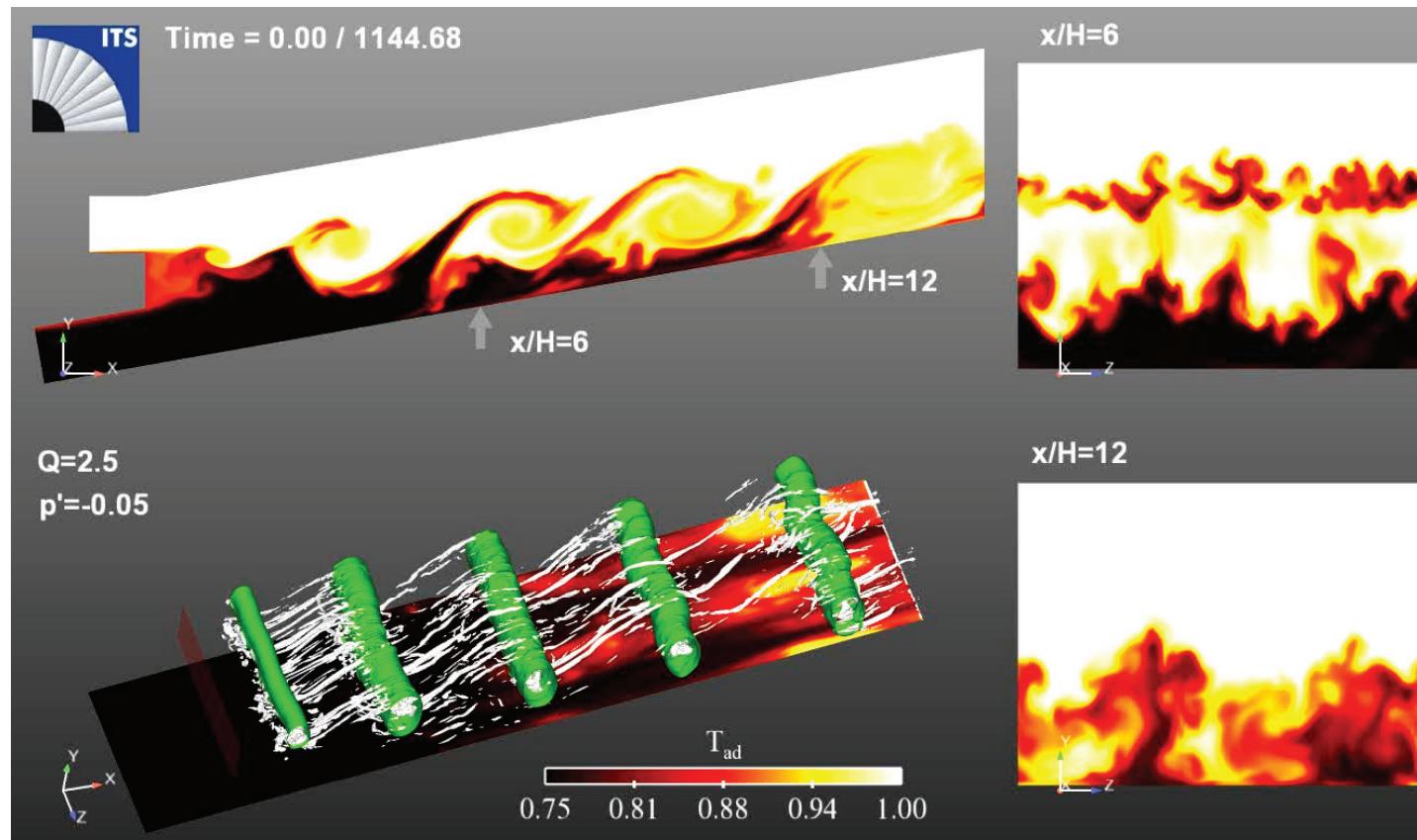
filename: 03HK_LES_M1.1_run4_4views.avi



Project: Trailing-edge cutback film-cooling

with Schneider & Bauer

Impact of coherent structures on the instantaneous flow and temperature field at the cutback for low blowing ratio with turbulent coolant ejection



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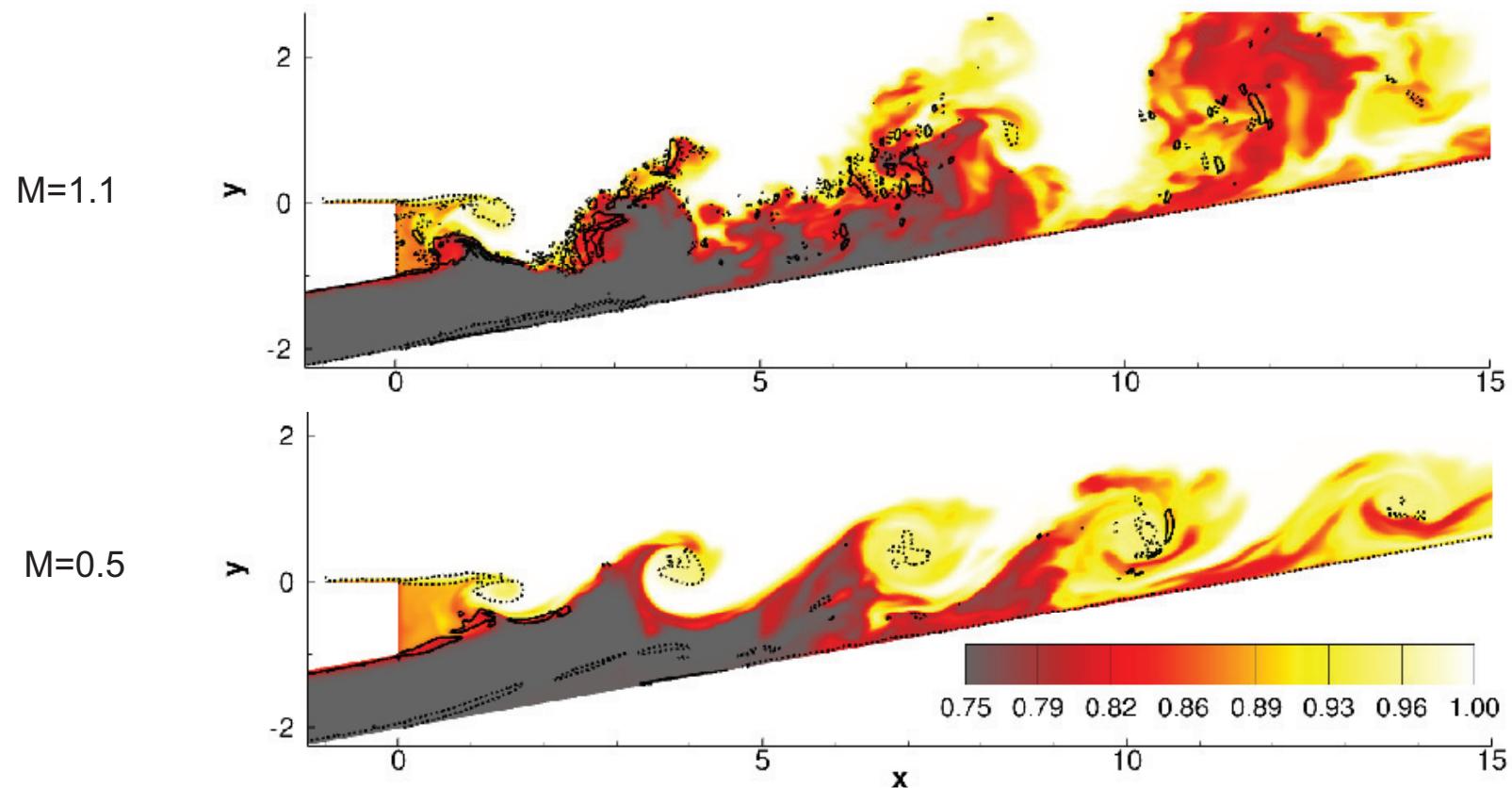
filename: 03HK_LES_M0.5_run2_4views.avi



Project: Trailing-edge cutback film-cooling

with Schneider & Bauer

Difference in coherent structures for turbulent coolant cases (largest scales)



color contours of temperature and contour lines of spanwise vorticity (dashed for negative values)

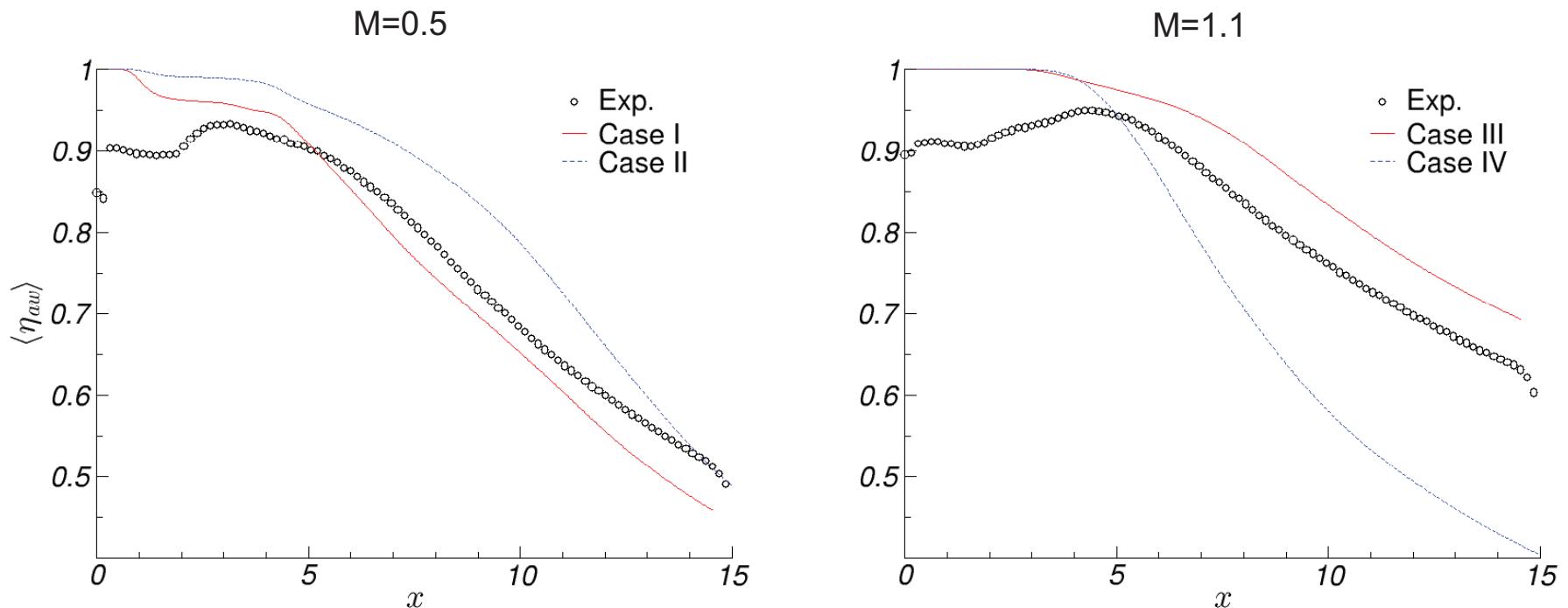


Project: Trailing-edge cutback film-cooling

with Schneider & Bauer

Effect on mean wall temperature:

Adiabatic film cooling effectiveness at different blowing ratios
for **laminar** and fully-developed **turbulent** coolant channel flow



Experimental data from Martini *et al.* (2006)



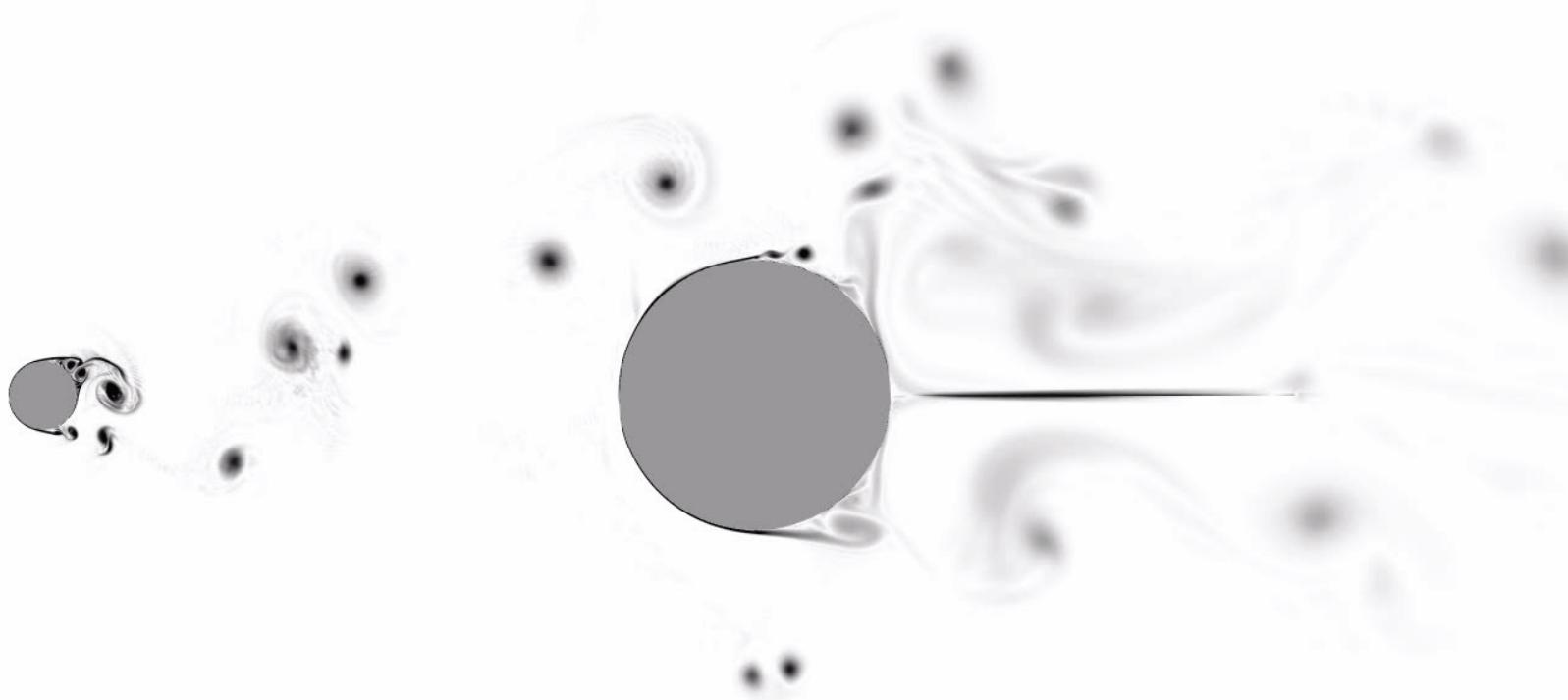
Conclusions

- DNS is a powerful tool with **high potential** for investigating unsteady heat transfer and fluid flow phenomena, in particular for cases involving transition to turbulence and/or large coherent structures
- DNS of idealized configurations related to turbomachinery components is already **possible**
- For more realistic configurations and the inclusion of more effects, reduction of computational cost is key issue (e.g., **hybrid methods**)
- Approach pursued here: **Embedded DNS**
(segregated coupling of DNS with LES and / or RANS)
- Embedded DNS is an **enabling technology** for many studies
- Pre-transitional heat transfer and trailing-edge cutback film-cooling are **good candidates for (embedded) DNS studies**

**THANKS TO ROLLS-ROYCE DEUTSCHLAND
AND DFG FOR SHARING THE VISION**



Thanks – Questions?



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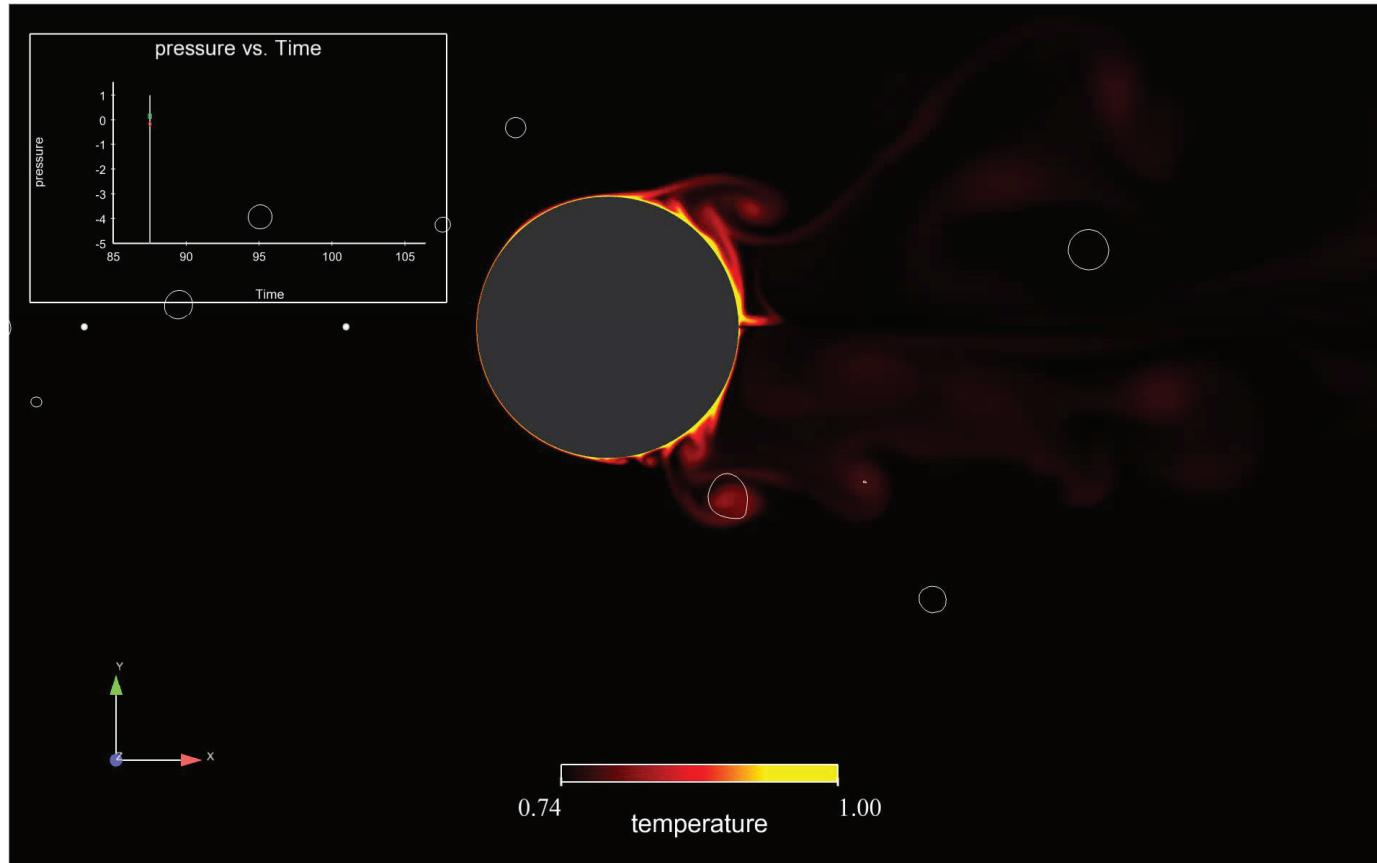
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Project: Pre-transitional heat transfer

with Venema & Rodi

Instantaneous temperature and spanwise vorticity contours



Coarse simulation (two-dimensional)

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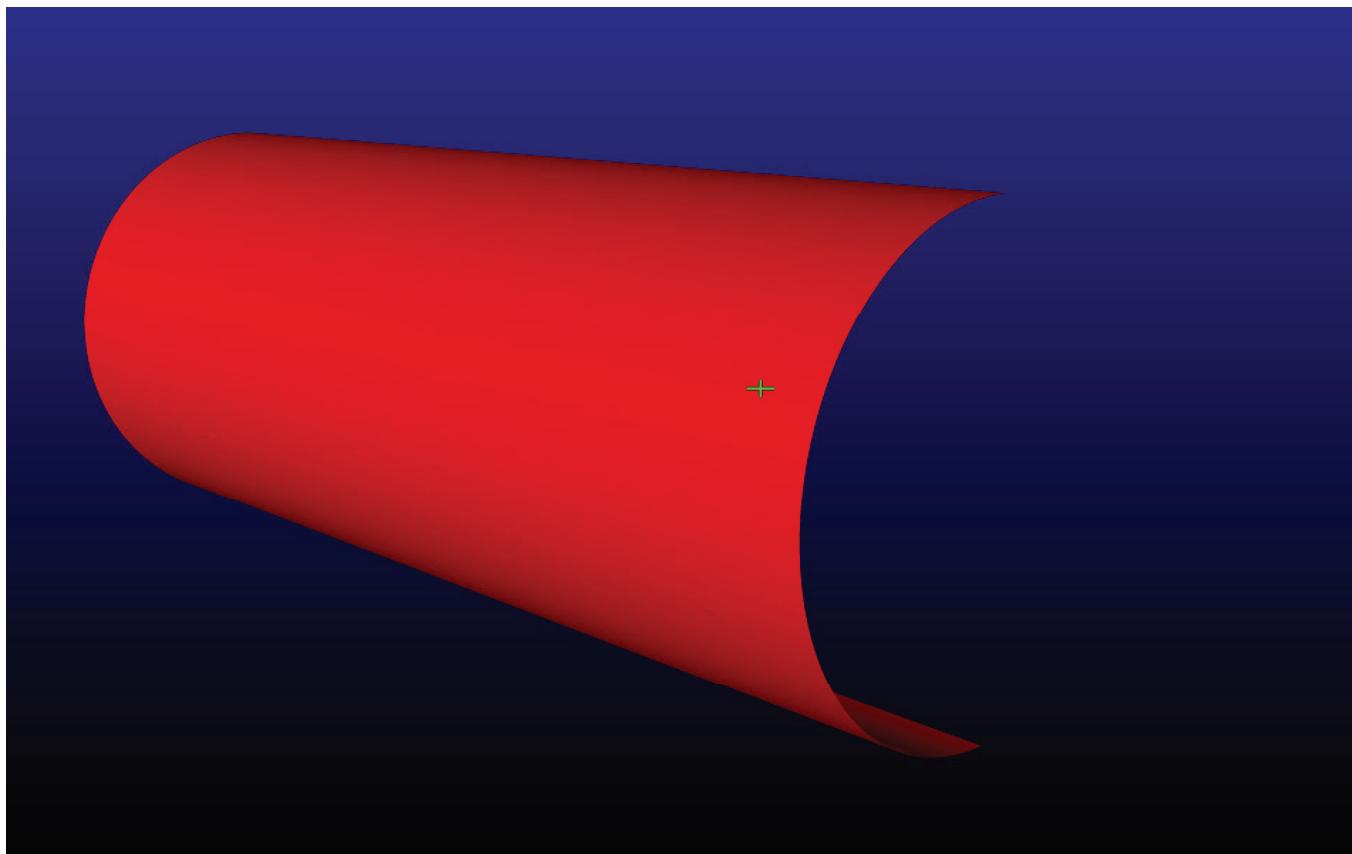
filename: 03t_p_isoccont_dc_re48000.avi



Project: Pre-transitional heat transfer

with Venema & Rodi

Instantaneous temperature contours (wall-adjacent cell at large heated cylinder)



Coarse simulation (full domain)

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filename: 03iso_temp.avi

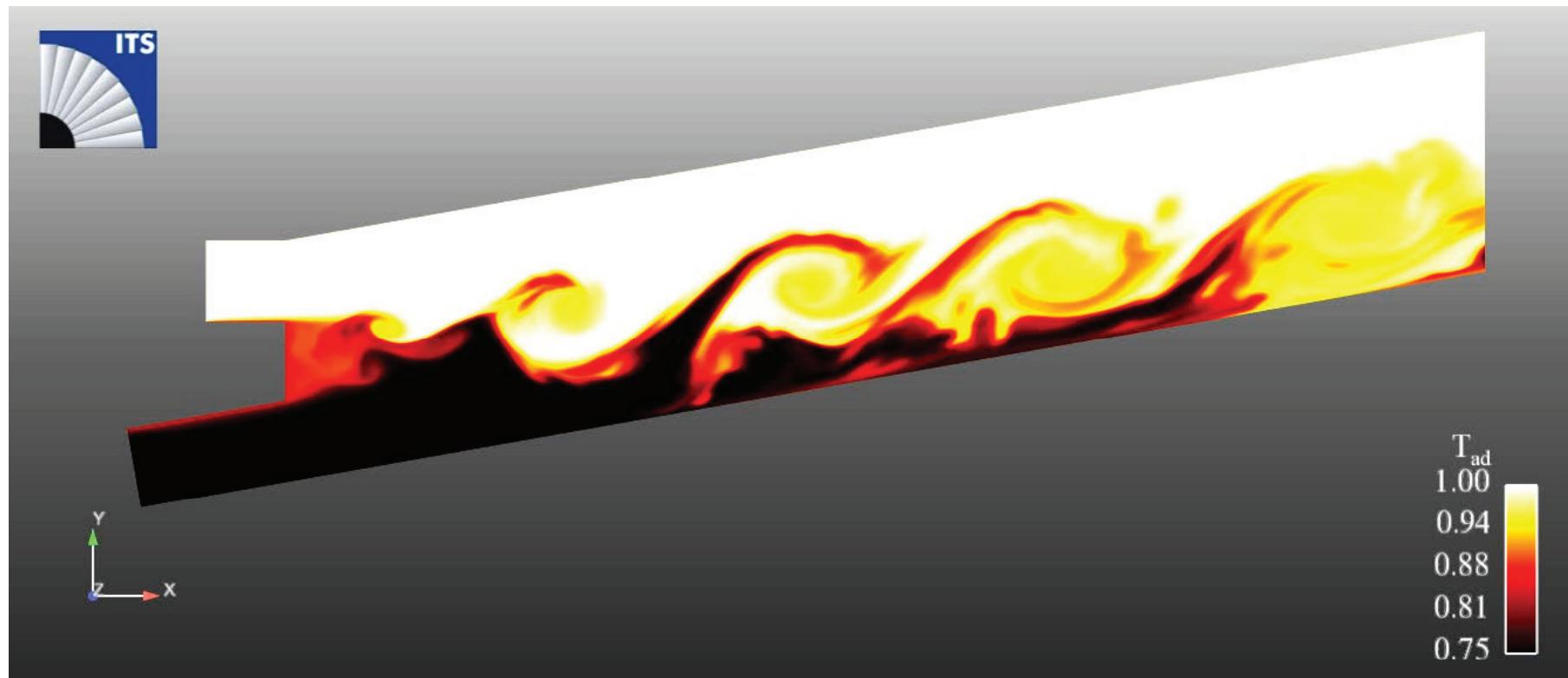


Project: Trailing-edge cutback film-cooling

with Schneider & Bauer

Impact of coherent structures on the instantaneous flow and temperature field at the cutback for low blowing ratio with turbulent coolant ejection

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filename: 03hk_movie_aiteb.avi

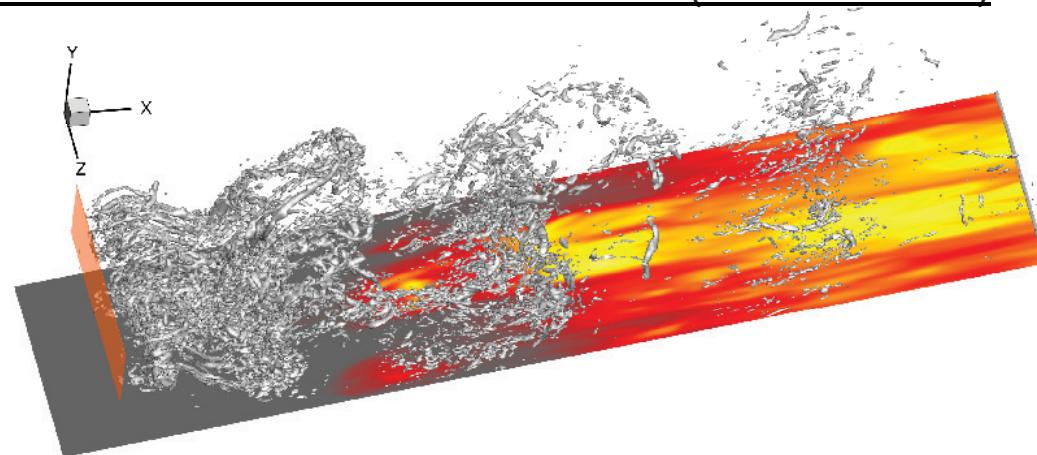


Project: Trailing-edge cutback film-cooling

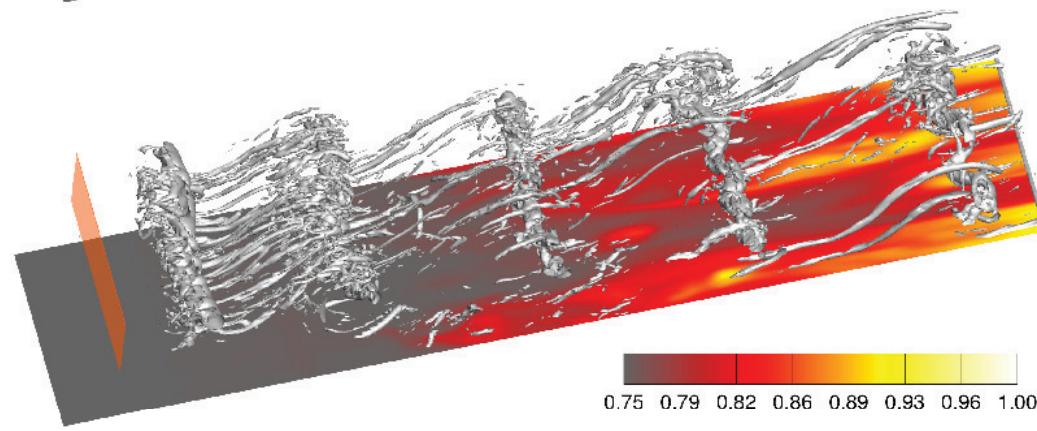
with Schneider & Bauer

Difference in coherent structures for turbulent coolant cases (smaller scales)

M=1.1



M=0.5



color contours of temperature in wall-adjacent cells and iso-contour of vortex identification criterion Q



What is DNS – vis à vis LES and RANS ?

Direct Numerical Simulation (DNS)

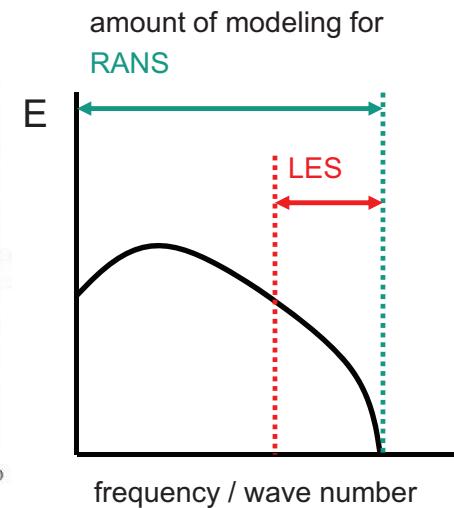
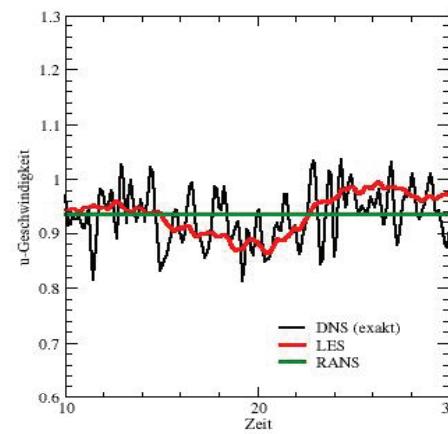
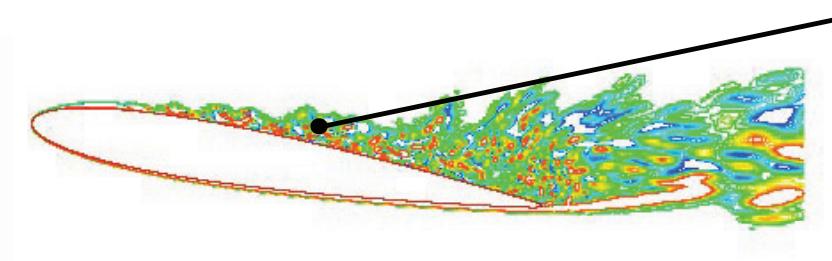
- solves numerically without turbulence modeling assumptions the governing (Navier-Stokes) equations
- all scales of motion must be resolved \Rightarrow extreme resolution requirements

Large Eddy Simulation (LES)

- computes large-scale motion directly
- model required to account for small-scale motion

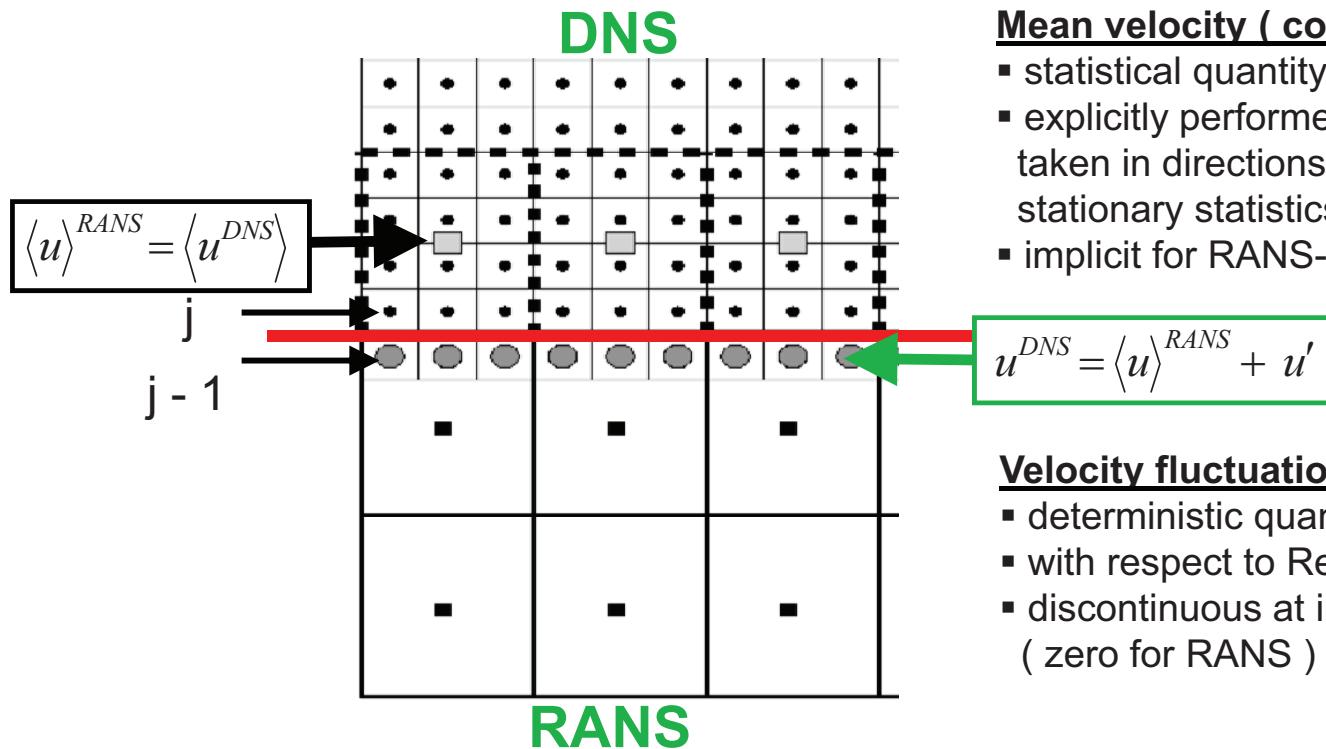
Reynolds-Averaged Navier-Stokes (RANS) Simulation

- provides only statistical information of the flow
- model required to account for all fluctuations



Key issue: Generation of fluctuations

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Mean velocity (coupled):

- statistical quantity (Reynolds average)
- explicitly performed on DNS-side and taken in directions with homogeneous / stationary statistics
- implicit for RANS-side

$$u^{DNS} = \langle u \rangle^{RANS} + u'$$

Velocity fluctuation (for DNS only):

- deterministic quantity
- with respect to Reynolds-average
- discontinuous at interface
(zero for RANS)

Inflow: variations of standard turbulent inflow data generators, e.g. digital filtering, rescaling, etc.
Outflow: enrichment [Quéméré & Sagaut, 2002] or convective coupling [von Terzi & Fröhlich, 2007]



Effect of the interface

Instantaneous u-velocity contours of a turbulent channel flow ($Re_\tau = 395$):

